

## INFLUENCE OF TITANIA ON PHASE COMPOSITION AND SELF-POWDER AND ALUMINA LEACHING PROPERTIES OF CALCIUM ALUMINATE SLAG

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### Abstract

The influence of  $\text{TiO}_2$  on the phase composition, self-powder and alumina leaching properties of calcium aluminate slag was investigated by XRD, laser particle size analyzer and chemistry analysis methods, and the measure of eliminating the adverse impacts of  $\text{TiO}_2$  on calcium aluminate slag was proposed. The results show that when the mass percent of  $\text{TiO}_2$  is 2% or less than 2%, the main phases of slag are  $\text{Ca}_{12}\text{Al}_{14}\text{O}_{33}$  and  $\gamma\text{-Ca}_2\text{SiO}_4$ , the self-powder rate of slag is above 95%, the alumina leaching rate is above 85%. The alumina leaching rate is gradually decreased when the  $\text{TiO}_2$  content is above 2%, the leaching rate is 80.1% with 3% of  $\text{TiO}_2$ , and the leaching rate is only 73.4% with 5% of  $\text{TiO}_2$ . To add CaO into containing 5%  $\text{TiO}_2$  of slag, the alumina leaching rate is 84.1% when the mole ratio of CaO added to  $\text{TiO}_2$  is 1.25, the adverse effects of  $\text{TiO}_2$  on the slag is basically eliminated, the calcium aluminate slag meets alumina leaching requirements.

### Introduction

The main phases of calcium aluminate slag are  $\gamma\text{-Ca}_2\text{SiO}_4$  and  $\text{Ca}_{12}\text{Al}_{14}\text{O}_{33}$ . Because the volume of slag can expand at 12% to make the slag powder when  $\beta\text{-Ca}_2\text{SiO}_4$  changes into  $\gamma\text{-Ca}_2\text{SiO}_4$  during the cooling process, so it is called self-powder slag. The  $\text{Ca}_{12}\text{Al}_{14}\text{O}_{33}$  and  $\text{CaAl}_2\text{O}_4$  in calcium aluminate slag can dissolve in sodium carbonate solution to produce sodium aluminate solution and calcium carbonate, and then alumina is extracted from the sodium aluminate solution. Simultaneously, because of slag self-powder, it has advantages that it can cancel the fragmentation process of raw materials and reduce costs. So since the 1970s, many scholars have studied to deal with the low-grade or refractory bauxite and secondary resources of containing aluminum by sintering or smelting reduction methods to obtain the calcium aluminate slag, and the alumina is extracted from the slag<sup>[1-5]</sup>.

The phase composition can effect the self-powder and alumina leaching properties of slag, while the material ratio of calcium aluminate slag is also an important factor of impacting on the phase composition. Many correlation studies of the impacting of the material ratio on the calcium aluminate slag have been done by researchers in domestic and foreign<sup>[6-12]</sup>. Barr researched the andalusite ore and believed that the best mole ratio of CaO to  $\text{Al}_2\text{O}_3$  (for short C/A) was from 1.3 to 1.66. Nielsen thought that the mass ratio of  $\text{Al}_2\text{O}_3$  to  $\text{SiO}_2$  (for short A/S) of raw materials should not be less than 5.5, otherwise it would reduce the leaching rate of  $\text{Al}_2\text{O}_3$ . Jingdong Zhang et al pointed out that the A/S of raw material had little impact on the leaching rate of  $\text{Al}_2\text{O}_3$ . Zhifang Tong synthesized the calcium aluminate slag with mixing CaO,  $\text{SiO}_2$  and  $\text{Al}_2\text{O}_3$  at the different ratios, and the results showed that the slag had better self-powder and leaching

properties when C/A was range from 1.6 to 1.8, and A/S was range from 0.5 to 1.5. Although the above research on calcium aluminate slag were more, but the studies mainly focused on the CaO- $\text{Al}_2\text{O}_3$ - $\text{SiO}_2$  system. The research report of the effect of the other components on calcium aluminate slag is few. There are many other element in actual slag, so each other effect of other composition will impact the phase composition of calcium aluminate slag.

The comprehensive utilization of high iron-containing red mud in Pingguo plant could be realized through the following process: firstly recovery of iron by smelting reduction method, then recovery of alumina by leaching the calcium aluminate slag obtained in smelting reduction process, and finally recovery of the other elements enriched in the leaching residue.

Pingguo red mud contains a certain proportion of  $\text{TiO}_2$ <sup>[13-14]</sup>, which can enter into slag in smelting reduction process, and effects on phase composition, self-powder and alumina leaching properties of calcium aluminate slag, at present, the research reports about this field is lack. In this paper, the influence of  $\text{TiO}_2$  on phase composition, self-powder and alumina leaching performances of calcium aluminate slag was investigated, and the measure of eliminating adverse effects of  $\text{TiO}_2$  on slag was proposed, and to provide the corresponding theoretical basis for comprehensive utilization of high iron-containing red mud.

### Experimental procedure

The raw materials are CaO,  $\text{Al}_2\text{O}_3$ ,  $\text{SiO}_2$  and  $\text{TiO}_2$  of analytical grade. The experimental slags were prepared by grinding and mixing uniformly according to a certain condition that the mole ratio of CaO to  $\text{SiO}_2$  (for short  $n(\text{CaO})/n(\text{SiO}_2)$ ) is 2, A/S is 0.8, thr mole ratio of CaO to  $\text{Al}_2\text{O}_3$  (for short  $n(\text{CaO})/n(\text{Al}_2\text{O}_3)$ ) is 1.71, the mass fraction of  $\text{TiO}_2$  is 1%, 2%, 3%, 4%, 5%, 6%, respectively. The slag was placed in graphite crucible, and placed in high-temperature molybdenum disilicide resistance furnace to melt. Melting temperature is 1500°C, holding time is one hour, and then cool the slag to 1200°C at the cooling rate of 4-5°C · min<sup>-1</sup> in the furnace, then put the slag out of furnace to cool in air, and to test the slag.

Slag leaching: Prepare the adjustment fluid with NaOH,  $\text{Na}_2\text{CO}_3$  of AR and  $\text{Al}(\text{OH})_3$  of industrial grade, in which the concentration of  $\text{Na}_2\text{O}_K$  is 7g · L<sup>-1</sup>,  $\text{Al}_2\text{O}_3$  is 7g · L<sup>-1</sup>,  $\text{Na}_2\text{O}_C$  is 110g · L<sup>-1</sup>. Accurately measure 150 ml adjusting liquid for the conical flask, and preheat it to 75°C in constant temperature water bath box with the magnetic stirring, and then put the 10g of slag into the conical flask to leach with constant agitation rate. Leaching time is 100 minutes, then to filter and analyze content of

Al<sub>2</sub>O<sub>3</sub> in filter slag by chemical analysis method, and calculate the Al<sub>2</sub>O<sub>3</sub> leaching rate of slag. The phase of slag was investigated using X-ray diffraction (Philips PW 3071 diffractometer with Cu K $\alpha$  radiation), the particle size distribution of slag using LS800 laser particle size analyzer. Through particle size distribution to analyze self-powder property (proportion of particles diameter less than 74 $\mu$ m)

## Results and discussions

### Effect of TiO<sub>2</sub> on phase in CaO-Al<sub>2</sub>O<sub>3</sub>-SiO<sub>2</sub> system slag

The phase composition of slag with the mass percent of TiO<sub>2</sub> from 1% to 6% was analyzed by an X-ray diffraction, and the results are shown in figure 1.

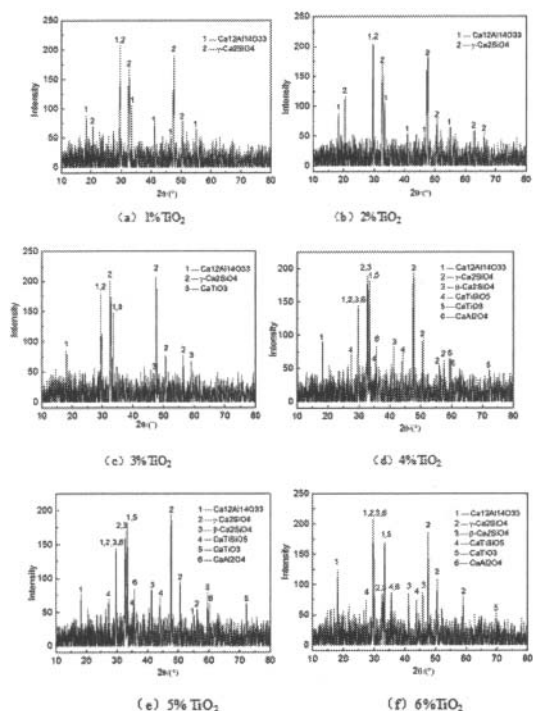


Fig.1 Effect of TiO<sub>2</sub> on phase composition of CaO-Al<sub>2</sub>O<sub>3</sub>-SiO<sub>2</sub> system

The figure 1 shows that when the mass fraction of TiO<sub>2</sub> is 1% and 2%, the main phases attained are Ca<sub>12</sub>Al<sub>14</sub>O<sub>33</sub> and  $\gamma$ -Ca<sub>2</sub>SiO<sub>4</sub>, and the phase containing titanium is not found. When TiO<sub>2</sub> increase to 3%, the main phases formed are Ca<sub>12</sub>Al<sub>14</sub>O<sub>33</sub>,  $\gamma$ -Ca<sub>2</sub>SiO<sub>4</sub> and a small amount of CaTiO<sub>3</sub>. When TiO<sub>2</sub> is 4%, the phases are Ca<sub>12</sub>Al<sub>14</sub>O<sub>33</sub>,  $\gamma$ -Ca<sub>2</sub>SiO<sub>4</sub>,  $\beta$ -Ca<sub>2</sub>SiO<sub>4</sub>, CaTiO<sub>3</sub>, CaTiSiO<sub>5</sub> and CaAl<sub>2</sub>O<sub>4</sub>. Increase TiO<sub>2</sub> to 5% and 6%, the phase composition have not changed.

### Effect of TiO<sub>2</sub> on self-powder and alumina leaching properties of CaO-Al<sub>2</sub>O<sub>3</sub>-SiO<sub>2</sub> system slag

The particle size distribution of synthetic slag with the mass percent of TiO<sub>2</sub> from 0% to 6% were analyzed, then through particle size distribution to analyze slag self-powder rate, and

through alumina leaching experiment to study effect of TiO<sub>2</sub> on alumina leaching property of slag, the results are shown in Figure 2.

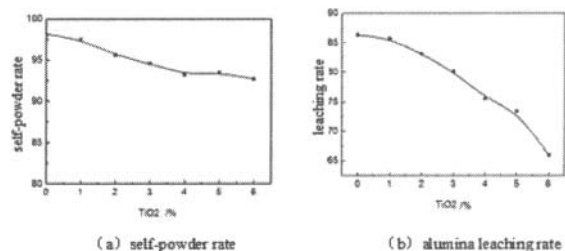


Fig.2 Effect of TiO<sub>2</sub> on self-powder rate and alumina leaching rate of slag

It can be seen from Figure 2 that the self-powder and alumina leaching rate of slag are gradually lowered with the mass percent of TiO<sub>2</sub> increase. The self-powder rate is gradually lowered from 98.1% to 92.7% with TiO<sub>2</sub> from 0% to 6%. When TiO<sub>2</sub> is 1% and less than 1%, the leaching rate is more than 85%. When TiO<sub>2</sub> is greater than 2%, the leaching rate is significant decreased with TiO<sub>2</sub> increasing, the leaching rate was 80.1% when TiO<sub>2</sub> is 3%, the leaching rate was only 66% when TiO<sub>2</sub> is 6%.

Combine figure 2 with the phase analysis in Figure 1 to discuss the change rules of the self-powder and leaching rate of slag. When the content of TiO<sub>2</sub> is above 4%, TiO<sub>2</sub> could enter into  $\beta$ -Ca<sub>2</sub>SiO<sub>4</sub> lattice and form a certain amount of solid solution phase of CaTiSiO<sub>5</sub> in slag cooling process, which could prevent change of part of the  $\beta$ -Ca<sub>2</sub>SiO<sub>4</sub> to  $\gamma$ -Ca<sub>2</sub>SiO<sub>4</sub>, and lead to slag self-powder rate decreased. When TiO<sub>2</sub> is less than 2%, the influence of TiO<sub>2</sub> on phase formation of slag is not significantly, the main phases formed are  $\gamma$ -Ca<sub>2</sub>SiO<sub>4</sub> and Ca<sub>12</sub>Al<sub>14</sub>O<sub>33</sub> which is easily for alumina leaching, so the alumina leaching rate of slag is more higher. When TiO<sub>2</sub> is above 4%, because TiO<sub>2</sub> combine with CaO, and form CaTiO<sub>3</sub>, and consume a certain amount of CaO, and lead to cause the content of CaO deficiency which can not be satisfied demand of combined with Al<sub>2</sub>O<sub>3</sub> to form Ca<sub>12</sub>Al<sub>14</sub>O<sub>33</sub>, so there is a certain amount of CaAl<sub>2</sub>O<sub>4</sub> formed in slag. Because Ca<sub>12</sub>Al<sub>14</sub>O<sub>33</sub> is more easily to extract alumina than CaAl<sub>2</sub>O<sub>4</sub>, so alumina leaching rate of slag is decreased gradually with the increase of the TiO<sub>2</sub> content.

### Effect of adding CaO for TiO<sub>2</sub> on CaO-Al<sub>2</sub>O<sub>3</sub>-SiO<sub>2</sub>-TiO<sub>2</sub> system

Because TiO<sub>2</sub> can combine with CaO to form CaTiO<sub>3</sub>, so that the prime ratio of n(CaO)<sub>2</sub>/n(Al<sub>2</sub>O<sub>3</sub>) changes and decreases, and lead to CaO deficiency and form a certain amount of CaAl<sub>2</sub>O<sub>4</sub>, and to decrease the alumina leaching rate. Therefore, through adding CaO for TiO<sub>2</sub> in slag, in order to change phase composition of slag, and to improve each property of slag.

Under the conditions that n(CaO)<sub>1</sub>/n(SiO<sub>2</sub>) is 2, m(Al<sub>2</sub>O<sub>3</sub>)/m(SiO<sub>2</sub>) is 0.8, n(CaO)<sub>2</sub>/n(Al<sub>2</sub>O<sub>3</sub>) is 1.71, the mass fraction of TiO<sub>2</sub> is 5%, add CaO for TiO<sub>2</sub> and make the mole ratio of CaO added to TiO<sub>2</sub> (for short n(CaO)<sub>3</sub>/n(TiO<sub>2</sub>)) be 0, 1.25, 1.5, 2.0, respectively. Investigate the influence rules of different n(CaO)<sub>3</sub>/n(TiO<sub>2</sub>) on phase composition, self-powder rate, alumina leaching rate of slag, the results of phase analysis are shown in figure 3, the results of self-powder and alumina leaching rate are shown in figure 4.

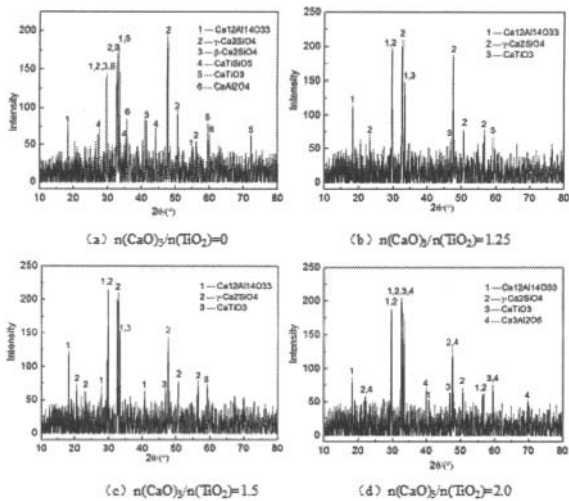


Fig.3 Effect of  $n(\text{CaO})_3/n(\text{TiO}_2)$  on phase composition of  $\text{CaO-Al}_2\text{O}_3\text{-SiO}_2\text{-TiO}_2$  system

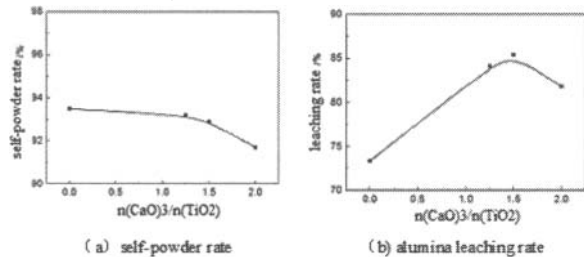


Fig.4 Effect of  $n(\text{CaO})_3/n(\text{TiO}_2)$  on self-powder rate and alumina leaching rate of slag

As shown in Figure 3, With  $n(\text{CaO})_3/n(\text{TiO}_2)$  increasing, the phase of  $\text{CaAl}_2\text{O}_4$  disappears. When  $n(\text{CaO})_3/n(\text{TiO}_2)$  is 1.25 and 1.5, respectively, the main phase formed are  $\text{Ca}_{12}\text{Al}_{14}\text{O}_{33}$  and  $\gamma\text{-Ca}_2\text{SiO}_4$ , in addition to a small amount of  $\text{CaTiO}_3$ . When  $n(\text{CaO})_3/n(\text{TiO}_2)$  increases to 2, there is a new phase of  $\text{Ca}_3\text{Al}_2\text{O}_6$  formed.

Figure 4 shows that the self-powder rate of slag decrease with the increases of  $n(\text{CaO})_3/n(\text{TiO}_2)$ . When  $n(\text{CaO})_3/n(\text{TiO}_2)$  is 2, the self-powder rate is lowest and 91.7%. Along with the  $n(\text{CaO})_3/n(\text{TiO}_2)$  increases, the leaching rate increase firstly and then decrease. The leaching rate is 84.1% when  $n(\text{CaO})_3/n(\text{TiO}_2)$  is 1.25, the leaching rate increase slightly and is 85.4% when  $n(\text{CaO})_3/n(\text{TiO}_2)$  is 1.5, continue to increase  $n(\text{CaO})_3/n(\text{TiO}_2)$  to 2, the leaching rate decrease to 81.8%.

Combine figure 4 with the phase analysis in Figure 3, it can be seen that with the content of  $\text{CaO}$  added increasing, the phase of  $\text{CaAl}_2\text{O}_4$  disappear gradually, and the alumina leaching rate improve significantly from 73.4% of no adding  $\text{CaO}$  to 84.1% of 1.25 of  $n(\text{CaO})_3/n(\text{TiO}_2)$ . It is reason that  $\text{CaO}$  added can make  $n(\text{CaO})_2/n(\text{Al}_2\text{O}_3)$  increase to promote phase of  $\text{Ca}_{12}\text{Al}_{14}\text{O}_{33}$  formation, which has the better leaching properties, and significantly reduce the adverse effects of  $\text{TiO}_2$  on slag. When  $n(\text{CaO})_3/n(\text{TiO}_2)$  is 2, the amounts of  $\text{CaO}$  added is excessive, the

worst leaching performance of phase of  $\text{Ca}_3\text{Al}_2\text{O}_6$  is formed, and lead to the leaching rate decline. Therefore, when  $n(\text{CaO})_3/n(\text{TiO}_2)$  is 1.25, the calcium aluminate slag basically meets alumina leaching requirement.

## Conclusions

The influence of  $\text{TiO}_2$  on phase composition, the self-powder and alumina leaching properties of calcium aluminate slag was ascertained. The measure to eliminate the adverse effects  $\text{TiO}_2$  on slag was proposed.

In  $\text{CaO-Al}_2\text{O}_3\text{-SiO}_2\text{-TiO}_2$  system, when the mass percent of  $\text{TiO}_2$  is less than 2%, the main phase formed are  $\text{Ca}_{12}\text{Al}_{14}\text{O}_{33}$  and  $\gamma\text{-Ca}_2\text{SiO}_4$ , the self-powder rate of slag is above 95%, the alumina leaching rate is greater than 85%. When the mass fraction of  $\text{TiO}_2$  is greater than 2%, the leaching rate decreased obviously with the increase of  $\text{TiO}_2$ , the leaching rate is only 73.4% when the content of  $\text{TiO}_2$  is 5%. For 5% of  $\text{TiO}_2$  of slag, through adding  $\text{CaO}$  for  $\text{TiO}_2$ , the alumina leaching rate of slag is 84.1% when  $n(\text{CaO})_3/n(\text{TiO}_2)$  is 1.25, and the adverse effects of  $\text{TiO}_2$  on slag are basically eliminated, and the calcium aluminate slag meets alumina leaching requirement.

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## References

1. Northeast University of Technology, Institute of aluminum and magnesium design of Shenyang <Study of Comprehensive utilization of high-iron bauxite of Guigang in Guangxi province> Identification of material, 1991: 6-8
2. Zhang Jingdong, Li Yinta, Bi Shiwen. Comprehensive utilization of high-iron bauxite of Guigang in Guangxi province [J].Light Metal, 8(1992):16-18
3. Bi Shiwen, Yang Yihong, Li Yitai. Extraction of aluminum from Calcium aluminate slag of the blast furnace [J].Light Metal, 6(1992):10~15
4. Tong Zhifang.Study of Comprehensive utilization of high-iron bauxite of Guigang in Guangxi province [D].Northeastern University, 2005:3~6
5. Grzymek J. Derdacka A. Konik Z. Method for obtaining aluminum oxide [P]. U.S. Patent: 4149898, 1978.
6. Barr L K. Alumina production from andalusite by the Pedersen process [M].Stockholm:Almqvist & Wiksell International. 1977:64-70
7. Nielsen K. The Pedersen processian old process in new light [J]. Erzmetall, 31(1978):523~525
8. Wang Bo, Yu Haiyan, Sun Huilan, Bi Shiwen. Effect of raw material mixture ratio on leaching and self-disintegrating behavior of calcium aluminate slag[J]. Northeastern University, 29(2008):1593-1596.
9. Grymek J. Influence of the structure of calcium aluminate on the process of manufacturing of metallurgical  $\text{Al}_2\text{O}_3$  from nonbauxitic aluminosilicate raw materials[J]. Scientific Bulletins of Lodz Technical University, 19(1986): 48~57

10. Grymek J. Complex production of aluminium oxide and iron from laterite raw materials applying the calcium aluminates polymorphism[C].Light Metals. New York: TMS, 1985:87~99
11. Grymek J, Derdacka A. Some physicochemical properties of  $12\text{CaO}\cdot 7\text{Al}_2\text{O}_3$  phase in relation to  $\text{Al}_2\text{O}_3$  production from self-disintegration sinters[C].Light Metals. Warrendale: TMS, 1987:91~97
12. Zhifang Tong.Effects of Cooling System and Raw Material Mixture Ratio on the Physical and Chemical Properties of Calcium Aliminum Slag[J].Nonferrous Metals Science and Engineering,4(2011):7~10
13. Jiang Yi-jiao, Ning Ping. Comprehensive Utilization of Red Mud in Alumina Plant [J].Environmental Science & Technology, 1(2003):15~17
14. Li Chaoxiang. The success of semi-industrial test that recycling of iron from Pingguo red mud [J]. Mining and Metallurgical Engineering, 20(2000):58~61