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# GROWTH MECHANISMS OF INTERMETALLIC PHASES IN DC CAST AA1XXX ALLOYS

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#### Abstract

In DC cast AA1xxx alloys, the presence of a fir-tree zone has long been recognized to be detrimental to the surface quality of critical sheet products. The fir-tree zone in DC cast ingots is mainly caused by a macroscopic transition between intermetallic phases. In this paper, the formation of major intermetallic phases commonly occurring in the DC ingot structure, such as Al<sub>3</sub>Fe, Al<sub>6</sub>Fe, Al<sub>m</sub>Fe and  $\alpha$ -AlFeSi, is investigated by using deep-etching and SEM techniques. The three-dimensional morphologies of intermetallic particles revealed by deep-etching are presented. Based on the morphological and growth kinetic aspects, the growth mechanisms of different intermetallic phases are discussed. The nucleation behaviors of intermetallics observed by SEM are also demonstrated.

# Introduction

Iron and Silicon are the most common impurities found in commercial AA1xxx aluminum alloys. It is known that iron has a high solubility in molten aluminum, but a very low one in the solid state. Therefore, almost all the iron in aluminum alloys forms intermetallic secondary phases. Silicon also has a partition coefficient of less than one and would be rejected into the liquid between dendrite arms during solidification. In combination with Si and Al, a large number of binary Al-Fe and ternary Al-Fe-Si intermetallic phases can precipitate while casting 1xxx alloys [1,2], depending on the solidification conditions and alloy chemistry. The types of intermetallic phases present in the cast structure can have a strong influence on the processing and final use properties of aluminum products.

In commercial purity alloys, the presence of the fir-tree zone has long been recognized to be detrimental to the surface quality of critical sheet products. Mainly caused by a macroscopic transition between intermetallic phases [3], the fir-tree zone is a macrodefect in the sub-surface regions of the DC cast ingot. The most commonly occurring intermetallic phases in DC cast 1xxx ingots are: monoclinic Al<sub>3</sub>Fe (the equilibrium phase, often designated as Al<sub>13</sub>Fe<sub>4</sub>), orthorhombic Al<sub>6</sub>Fe, tetragonal Al<sub>m</sub>Fe and cubic  $\alpha$ -AlFeSi [4]. The classical fir-tree was described as a transition from metastable Al<sub>6</sub>Fe to stable Al<sub>3</sub>Fe during solidification. More recently, it has been established [5-7] that the fir-tree zone can result from various other combinations involving different intermetallic phases such as  $\alpha$ -AlFeSi  $\rightarrow$  Al<sub>3</sub>Fe,  $\alpha$ -AlFeSi  $\rightarrow$  Al<sub>6</sub>Fe, and Al<sub>m</sub>Fe  $\rightarrow$  Al<sub>6</sub>Fe. Furthermore, there is evidence that the fir-tree zone does not exclusively represent a transition from one single phase to another. In cast ingots, there is often a mixture of intermetallic phases existing on both sides of the fir-tree zone and the balance and type of phases vary across the zone. Thus, it is of considerable technological interest to control the formation of Al-Fe and Al-Fe-Si phases in the ingot cast structure in order to eliminate the fir-tree defect.

The purpose of the present work is to investigate the growth morphologies and the nucleation behaviors of the major intermetallic phases that commonly occur in the DC cast AA1xxx ingot structure. Deep-etching and SEM techniques were utilized to determine the three-dimensional morphologies of different intermetallic phases.

# Experimental

Most samples were taken from commercial DC sheet ingots in the as-cast condition, and the examinations were carried out on the subsurface region (0-60 mm from cast surface) where the fir-tree zone appears. Some samples were made by a DC Simulator in which a small cylindrical sample with a diameter of 35 mm was cast under cooling conditions similar to DC ingots. The materials investigated were DC cast commercial purity alloys. The main work was performed on the two alloy groups with the composition ranges given in Table 1. The alloys in Group A, with low Si levels, were used to study the binary Al-Fe compounds, whereas examination of the ternary  $\alpha$ -AlFeSi phase concentrated on Group B, since the  $\alpha$ -AlFeSi becomes one of the major intermetallic phases in the structure only at higher Si levels.

	Fe	Si	Cu	Mn	Mg
Group A	0.25-0.35	0.05-0.15	< 0.03	< 0.03	< 0.03
Group B	0.30-0.40	0.25-0.35	< 0.03	< 0.03	< 0.03

Table I - Chemical Compositions of the Examined Aluminum Alloys (wt %)

To observe the three-dimensional morphologies of intermetallic particles, a deep-etching technique was applied. The basic idea of deep-etching is to dissolve the aluminum matrix in the surface layer of a sample without disturbing the secondary phases. The procedure is quite simple: a finely ground metallographic specimen was put into a 12% HCl solution for several minutes. Under SEM (secondary electron scanning image), the phase morphology in the cast structure can be studied *in situ*.

To confirm the phase type at various positions of a sample, an intermetallic extraction method (with butanol or phenol), combined with XRD analysis for phase identification [3,8], was used.

## **Results**

#### Phase Morphology

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#### Al<sub>3</sub>Fe

Under optical microscopy, the typical appearance of  $Al_3Fe$  is flaked and needle-like, and distributed along aluminum cell boundaries (Figure 1). Revealed by deep-etching, Figure 2 shows the three-dimensional view of  $Al_3Fe$  which is, in reality, plate-like. The  $Al_3Fe$  plate grows in a faceted manner with a preferred direction.

Sometimes in a polished section, it can be seen that a number of angular Al<sub>3</sub>Fe particles located in the interdendritic region and their distribution seems more or less irregular. Under SEM, it appears that many fine plates tend to form a cluster. By careful observation, it is found that the Al<sub>3</sub>Fe forms side branches on the surface of a plate at different angles and then connect each other in some extension (Figure 3). Examination, in a large number of sections, shows that the anglers between branched plates widely vary and no fixed relationships can be established.

#### Al<sub>m</sub>Fe

In DC ingot structures,  $Al_mFe$  is one of the frequently encountered metastable phases. It appears fibrous in a metallographic section (Figure 4), and as usual in dilute alloys, the particles locate in the cell boundaries. The SEM micrograph (Figure 5) shows  $Al_mFe$  exhibiting a fine feathery characteristic with many fibers growing in different orientations. Another SEM micrograph (Figure 6) shows a complex of  $Al_mFe$  over a few aluminum cells. The fine feathers or fibers of the  $Al_mFe$  can advance in a variety of curved forms and are able to branch frequently in order to achieve spacing adjustment and change of growth direction. Consequently, the  $Al_mFe$  connect each other in the interdendritic region over a wide range.



Figure 1: Photomicrograph of a DC ingot structure showing the flaked and needle-like Al<sub>3</sub>Fe.



Figure 2: SEM micrograph of a deep etched sample illustrating the plate-like morphology of  $Al_3Fe$ .



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Figure 3: SEM micrograph (deep etched) showing that  $Al_3Fe$  forms side branches.



Figure 6: A complex of  $Al_mFe$  in the three-dimensional view. The fine feathers or fibers of  $Al_mFe$  can advance in a variety of curved forms and connect each other in the interdendritic region over a wide range.



Figure 4: Photomicrograph of a DC ingot structure showing the fibrous  $Al_mFe$ .



Figure 5: SEM micrograph of a deep etched sample illustrating the fine feathery characteristic of  $Al_mFe$ .

## Al<sub>6</sub>Fe

Al<sub>6</sub>Fe is another metastable phase that commonly occurs in DC ingot structure. Figure 7 shows a micrograph of Al<sub>6</sub>Fe. Its typical appearance seems to be as a flake with several short wings. In a three-dimensional view, Al<sub>6</sub>Fe often shows a curved plate with a number of rod-like side branches (Figure 8). Observation of various samples shows that the fine branches of Al<sub>6</sub>Fe are faceted on the micro-scale, and that Al<sub>6</sub>Fe generally has a flexible branching ability. If the interdendritic space is large enough (at the corners of several aluminum cells), Al<sub>6</sub>Fe's form can become quite complicated. A skeleton-like morphology is occasionally observed.

## α-AlFeSi

In low Si 1xxx alloys, the common intermetallic phases are the three binary Al-Fe compounds mentioned above. With increased silicon content, the metastable  $\alpha$ -AlFeSi becomes one of the major phases in the ingot structure. The microstructural characteristic of  $\alpha$ -AlFeSi is the so-called "Chinese script" (Figure 9). Figure 10 shows the three-dimensional view of  $\alpha$ -AlFeSi. It looks like a complicated dendrite form. Within a complex of the particle, some plates are large and wide, while others are small and thin. Moreover, in some plates, the small platelets can grow directly from the sides of a large plate. This arrangement and the non-uniform spacing, probably cause the script image in a metallographic section. An important feature of the α-AlFeSi, that leads to distinguish it easily from the binary Al-Fe intermetallics, is the triangular edge on the front of each plate. These plates are certainly faceted. Another interesting point is that in the edge of a parent plate, another plate can nucleate, branch and further grow in various directions. In this way the  $\alpha$ -AlFeSi plates connect each other in the interdendritic region.

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Figure 7: Micrograph of  $Al_6Fe$  in a metallographic section (SEM in backscatter mode).



Figure 8: SEM micrograph (deep etched) showing that  $Al_6Fe$  often has a curved plate with a number of rod-like side branches.



Figure 9: Photomicrograph of  $\alpha$ -AlFeSi showing the script characteristic.



Figure 10: Three-dimensional view of  $\alpha$ -AlFeSi in the ingot structure (SEM, deep etched).

## Nucleation Behavior

In the deep etched samples, if an intermetallic particle is close and parallel to the cut surface, the nucleation site of the particles may occasionally be brought to light for observation.

#### Al<sub>m</sub>Fe

Figure 11 shows an  $Al_m$ Fe growth unit and its nucleation center. It is clear to see that the  $Al_m$ Fe phase grows from the center into its surroundings with numerous fine branched feathers or fibers. The site of the nucleation appears in the form of an agglomerate of a few small particles, that range from 0.2 to 1  $\mu$ m. SEM-EDS (energy dispersive spectrometer) analysis indicates that these particles are a high Ti-containing compound. The crystal structure of the compound is under further investigation.

Some observations were performed in a transition region where the plate-like Al<sub>3</sub>Fe are located on one side and the fine feathery  $Al_mFe$  on the other side. Figure 12 shows an example of how the  $Al_mFe$  nucleate and grow in this region. The appearance of the intermetallic particle here is very unique. The lower part of the particle is typically plate-like and relates to the stable  $Al_3Fe$  phase, whereas the upper part has a fine feathery characteristic and certainly belongs to the metastable  $Al_mFe$  phase. Since the  $Al_3Fe$  has a higher eutectic temperature than the  $Al_mFe$ ,  $Al_3Fe$  forms first in the interdendritic liquid during the solidification and then  $Al_mFe$  follows. The evidence of the picture indicates that the  $Al_mFe$  can nucleate from the already existing  $Al_3Fe$  and then grow further.

## Al<sub>6</sub>Fe

Figure 13 shows a growth unit and its nucleation site of Al<sub>6</sub>Fe. A small cubic particle (about 2  $\mu$ m) is found in the center area of the Al<sub>6</sub>Fe unit and from there the phase grows into its surroundings. SEM-EDS analysis indicates that the particle contains only two elements, mainly Al and a small amount of Fe. It is noted that after deep-etching, the surface of the  $\alpha$ -Al matrix always exhibits the cubic form of its crystallographic nature. The size of these cubes

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ranges within a few micrometers. Considering that the central particle is  $\alpha$ -Al and acts as an active nucleant for the Al<sub>6</sub>Fe, it could explain that some iron is picked up by the SEM-EDS analysis, since the Al<sub>6</sub>Fe phase would grow from certain planes of the  $\alpha$ -Al crystal.

In addition, Bäckerud [9] suggested that due to the orthorhombic crystal structure of Al<sub>6</sub>Fe, the low lattice disregistry can be well fitted between Al<sub>6</sub>Fe and  $\alpha$ -Al. Thus, it is reasonable to suppose that the nucleation site discovered in Figure 13 is  $\alpha$ -Al.



Figure 11: Nucleation center of Al<sub>m</sub>Fe in the ingot structure.



Figure 12: SEM micrograph (deep etched) showing the transition of  $Al_mFe$  from  $Al_3Fe$ .



Figure 13: A growth unit and its nucleation site of Al<sub>6</sub>Fe (SEM, deep etched).

## Discussion

In the binary Al-Fe system, Al<sub>3</sub>Fe is the only existing equilibrium phase. The entropy of fusion for Al<sub>3</sub>Fe is greater than 2 and it therefore tends towards faceted growth [10]. In DC casting at low cooling rates, Al<sub>3</sub>Fe grows as individual faceted plates with a preferred direction in the remaining eutectic liquid between  $\alpha$ -Al dendrites. The faceted plates are usually straight and unrelated. In this case, repeated nucleation is the only way for Al<sub>3</sub>Fe to maintain the continuity of the phase precipitation as solidification proceeds. At higher cooling rates, Al<sub>3</sub>Fe begins to branch, probably caused by twin or crystal faults [10]. Side plates can form on the surface of a parent plate through different angles. The branching permits the spacing adjustment between plates and a change of growth direction, although the branching ability of Al<sub>3</sub>Fe is somewhat limited in this way, less repeated nucleation is needed to allow continuous growth.

Our observation in the ingot structure shows that  $Al_mFe$  has fine feathery morphology and excellent branching ability. The edge of the fine branches, particularly at the growth front where it contacts with liquid, is round. Although no data of the entropy of fusion for  $Al_mFe$  is available, from the morphological viewpoint, it is obvious that the growth of  $Al_mFe$  is non-faceted.

In contrast to  $Al_mFe$ , the initial morphology of  $Al_6Fe$  is still platelike, which can be clearly seen from a growth unit with its initial point (Fig. 13). As the growth progresses, the rod-like or feathery branches appear and go further. However, the front edge of the rodlike  $Al_6Fe$  is still faceted. This was also observed by Adam and Hogen in 2-4% Fe aluminum alloys [11]. The entropy of fusion for  $Al_6Fe$  was reported to be around 2 [9,11]. It can therefore be concluded that the growth manner of  $Al_6Fe$  is between faceted and non-faceted. With an increase in cooling rate, the tendency to nonfaceted growth increases, resulting in the dominant rod-like growth of  $Al_6Fe$ . Similar to the analysis of  $Al_6Fe$ , the growth of  $\alpha$ -AlFeSi in the dilute Al-Fe-Si alloys is also between faceted and non-faceted, but is more likely to be in the faceted direction.

Since all four intermetallics have distinct morphologies and different growth modes, the growth kinetic of each intermetallic

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phase is quite different. Al<sub>3</sub>Fe has the slowest growth kinetic associated with its faceted and relatively rigid growth mode, whereas Al<sub>m</sub>Fe exhibits the highest growth kinetic due to its nonfaceted manner and excellent branching ability, providing a great growth advantage at high cooling rates (growth rates). The Al<sub>6</sub>Fe and  $\alpha$ -AlFeSi represent intermediate cases because of their transitional position between faceted and non-faceted.

The nucleation process and subsequent growth of individual intermetallics will control the phase selection, and thereby determine the fir-tree zone present in the ingot structure. The nucleation process is mainly dependent on the thermodynamic factor and the effectiveness of heterogeneous nucleants. The thermodynamic driving force for the formation of stable Al<sub>3</sub>Fe is always greater than that for the metastable phases, in a descending order of Al<sub>3</sub>Fe, Al<sub>6</sub>Fe and Al<sub>m</sub>Fe, since Al<sub>3</sub>Fe has a higher eutectic temperature than Al<sub>6</sub>Fe and Al<sub>m</sub>Fe. Although one phase may be favored thermodynamically over another phase, the potential nucleants for both phases could change the competition. For example, it is often seen in DC ingots that Al<sub>m</sub>Fe exists together with Al<sub>3</sub>Fe or even becomes the dominant phase in the shell zone where the cooling rate is the lowest in the sub-surface region of ingots. It is believed that efficient nucleants for Al<sub>m</sub>Fe, as discovered in the present work, play an important role in promoting Al<sub>m</sub>Fe in the shell zone.

On the other hand, the subsequent growth process is determined by local solidification conditions and growth modes of intermetallics. In general, as the cooling rate (growth rate) increases, the Al<sub>3</sub>Fe will be replaced by the Al<sub>6</sub>Fe and be further taken over by Al<sub>m</sub>Fe in the binary Al-Fe system. The growth mode of individual intermetallics will aid in understanding the phase selection during solidification. However, in dilute alloys, the eutectic reaction for formation of intermetallics takes place only in the last less than 10% of the remaining liquid. The local solidification conditions of the rest of the interdendritic liquid, particularly in the sub-surface region of ingots where the cooling rate and growth rate change dramatically, are often not available in detail, since the widely employed cell size and cooling rate measurements reflect mainly the primary  $\alpha$ -Al growth. As a result, studies of the phase selection in DC ingots related to the fir-tree defect have still been qualitative in nature.

#### Summary

In the present study, the growth morphologies of the four intermetallic phases, Al<sub>3</sub>Fe, Al<sub>6</sub>Fe, Al<sub>m</sub>Fe and  $\alpha$ -AlFeSi, were investigated in DC cast AA1xxx alloys. The two-dimensional image of intermetallics in a metallographic section and the three-dimensional view revealed by deep-etching were presented. It was found that all four intermetallic phases have distinct morphologies and growth kinetics. Based on the morphological and growth kinetic aspects, the characteristics and growth mechanisms of each phase in DC ingots were discussed.

The nucleation behaviors of some intermetallics were also studied. The heterogeneous nucleants of individual intermetallic phases could play an important role in the control of phase selections.

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# References

1. H. Westengen, "Formation of Intermetallic Compounds During DC Casting of a Commercial Purity Al-Fe-Si Alloy", Z. Metallkde. 73 (1982), 360-368.

2. P. Skjerpe, "Intermetallic Phases Formed During DC-Casting of an Al-0.25 Wt Pct Fe-0.13 Wt Pct Si Alloy", Met. Trans. A, 18A (1987), 189-200.

3. H. Kosuge, I. Mizukami, "Formation of 'Fir-tree' Structure in D.C. Cast Ingots of Al-0.06%Fe Alloys", J. Jap. Inst. L. Met., 25 (2) (1975), 48-58.

4. P. V. Evans et al., "Intermetallic Phase Selection in AA1xxx Aluminum Alloys", In: Proceedings of the 4<sup>th</sup> Decennial International Conference on Solidification Processing, Sheffield, July 1997, 531-535.

5. S. Brusethaug, D. Porter, O. Vorren, "The Effect of Process Parameters on the Fir-Tree Structure in DC-Cast Rolling Ingots", In: The 8th International Leichtmetalltagung, Leoben-Wien, 1987, 472-476.

6. H. Tezuka, A. Kamio, "Influence on Minor Elements on the Crystallization Manner of Intermetallic Phases in Unidirectionally Solidified Al-Fe Alloys", In: The 3rd International Conference on Aluminum Alloys, Vol. 1, 1992, 117-122.

7. S. J. Maggs et al., "The Effect of Trace Element on Intermetallic Phase Selection in Simulated DC Castings", Light Metals, 1995, 1039-1047.

8. A. K. Gupta, P. H. Marois, D. J. Lloyd, "Review of the Techniques for the Extraction of Second-phase Particles from Aluminum Alloys" Materials Characterization, 37(1996), no 2/3, 61-80.

9. L. Bäckerud, "Kinetic Aspects of the Solidification of Binary and Ternary Alloy Systems", Jernkontorets Annaler, 152 (1968), 109-138.

10. C. McL. Adam, L. M. Hogan, "Crystallography of the Al-Al $_3$  Fe Eutectic", Acta Met. 23(1975), 345-354.

11. C. McL. Adam, L. M. Hogen, "The Aluminum-Iron Eutectic System", J. Aust. Inst. Met. 17 (1972), 81-89.