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## Phase and Melting Relations of Fe<sub>3</sub>C to 300 GPa and Carbon in the Core

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### ABSTRACT

Carbon is a plausible candidate for a light element in the Earth's core. Here, we show that Fe<sub>3</sub>C melts incongruently to form Fe<sub>7</sub>C<sub>3</sub> and liquid at least up to 200 GPa based on in-situ X-ray diffraction measurements and textural observations of the recovered samples, and Fe<sub>3</sub>C is stable at least up to 300 GPa at high temperatures. The C content of the liquid coexisting with Fe<sub>7</sub>C<sub>3</sub> decreases and the Fe-Fe<sub>3</sub>C eutectic composition shifts toward the Fe-rich direction with increasing pressure. The present result revealed that both Fe<sub>3</sub>C and Fe<sub>7</sub>C<sub>3</sub> are plausible constituents in the inner core.

### 3.1. INTRODUCTION

Seismological studies (Dziewonski & Anderson, 1981) show that the inner core is less dense than pure iron under the core conditions (Mao et al., 1990); therefore, it has been accepted that the inner core comprises iron along with lighter elements (Birch, 1964; Poirier, 1994). The density deficit of the core is estimated to be 3%–10% for the outer core (Anderson & Isaak, 2002; Shanker et al., 2004) and 2.5%–9% for the inner core (Dubrovinsky et al., 2000; Dewaele et al., 2006). Carbon is one of the major candidates for the light elements contained in the Earth's core (Hirayama et al., 1993; Wood, 1993; Dasgupta & Walker, 2008; Chi et al., 2014) because carbon has a high abundance in the solar system (Anders & Grevesse, 1989) and it can dissolve significantly in

molten iron, even at ambient and upper mantle pressures (Wood, 1993; Dasgupta & Walker, 2008). Although several studies on the physical and chemical properties of iron carbides have been carried out at high pressure, there are still very limited numbers of experimental works on the phase and melting relationships in the Fe-C system to the core conditions.

Wood (1993) estimated the phase diagrams of the Fe-C system up to the pressure of the core mantle boundary (CMB) and suggested that about 2–4 wt.% of carbon could be stored in the core during the core formation stage. He suggested that the Earth's inner core is composed solely of Fe<sub>3</sub>C. Nakajima et al. (2009) reported the phase relationships in the Fe-C system up to 30 GPa based on textural observations, chemical analysis of the recovered samples, and in-situ X-ray diffraction experiments using a Kawai-type multianvil apparatus. According to Nakajima et al. (2009), Fe<sub>3</sub>C melts incongruently to form Fe<sub>7</sub>C<sub>3</sub> and a liquid phase at 30 GPa. They proposed that Fe<sub>7</sub>C<sub>3</sub> is present in the inner core. Lord et al. (2009) determined the melting temperatures of Fe<sub>3</sub>C and Fe<sub>7</sub>C<sub>3</sub> and the Fe-Fe<sub>3</sub>C eutectic temperature up to 70 GPa from the temperature plateau obtained while increasing the laser power in a laser-heated diamond anvil cell (DAC). However, there were obvious discrepancies between the melting curves of Fe<sub>3</sub>C and Fe<sub>7</sub>C<sub>3</sub>

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reported by Nakajima et al. (2009) and Lord et al. (2009). In addition, Lord et al. predicted that  $\text{Fe}_3\text{C}$  decomposes to Fe and  $\text{Fe}_7\text{C}_3$  and suggested that the inner core is composed of Fe +  $\text{Fe}_7\text{C}_3$ . On the other hand, Sata et al. (2010) reported that  $\text{Fe}_3\text{C}$  is stable up to at least 187 GPa at 300 K. In this study, high-pressure and high-temperature experiments using a double-sided laser-heated DAC were performed up to the pressure conditions of the inner core to investigate the phase and melting relationships of  $\text{Fe}_3\text{C}$ . The melting temperature of  $\text{Fe}_3\text{C}$  was determined from in-situ X-ray diffraction experiments and textural observations on recovered samples. This study aimed to reveal the phase and melting relationships of the Fe-C system under core conditions and to discuss carbon storage in the Earth's inner core.

### 3.2. EXPERIMENTAL PROCEDURE

We have conducted two types of experiments, in-situ X-ray diffraction experiments for determination of the phase and melting relations of  $\text{Fe}_3\text{C}$ , and a quenching experiment at 59 GPa and 2850K for textural observations of the recovered sample.

#### 3.2.1. Sample Preparations

The starting material for the in-situ X-ray diffraction experiments was a powdered sample of cementite  $\text{Fe}_3\text{C}$ , which was synthesized from a stoichiometric mixture of iron and graphite at 3 GPa and 1273 K for 12 h using a 3000-ton Kawai-type multianvil apparatus installed at Tohoku University. The synthesized  $\text{Fe}_3\text{C}$  was confirmed to be a single phase of cementite by X-ray diffraction and SEM observations, that is, it was a single phase of cementite  $\text{Fe}_3\text{C}$  without chemical zoning and interstitial phases.

The starting material used for the quench experiment was a mixture of Fe and  $\text{Fe}_3\text{C}$  synthesized by the above procedure. The powdered mixture was laser heated using a Nd:YAG laser ( $\lambda = 1.064 \mu\text{m}$ ) in an Ar atmosphere and quenched rapidly, forming a fine dendritic texture with a typical size  $<1 \mu\text{m}$ . The starting materials thus synthesized were analyzed based on the procedure by Dasgupta & Walker (2008) and Walker et al. (2013). After polishing the samples, the carbon content was analyzed using a wavelength-dispersive spectrometer with an EPMA (JXA-8800; JEOL, Tokyo, Japan). The calibration standard, which is cementite without zoning or interstitial phases synthesized at 3 GPa and 1273 K, was coated with aluminium. An acceleration voltage of 15 kV and a beam current of 90 nA were employed to analyze the carbon content. An LDE1H crystal in the EPMA was used to measure the carbon content in the sample. We used a defocused beam (50  $\mu\text{m}$  in diameter) to perform the

**Table 3.1** The compositions of the starting material for the quenched experiment, and the quenched liquid and coexisting  $\text{Fe}_7\text{C}_3$  recovered from 59.4 GPa and 2850 K. Numbers in parentheses are uncertainties on the last digits. The uncertainty of the composition of the quenched liquid is the compositional variation in the multiple analysis of the quenched melt region (see Figure 3.3).

		Fe (wt.%)	C (wt.%)	Total
Starting material		94.6 (3)	5.2 (4)	99.8
Recovered sample	$\text{Fe}_7\text{C}_3$	91.2 (1)	8.1 (1)	99.3
	Quenched liquid	93.9 (7)	4.7 (4)	98.6

quantitative analysis of the bulk starting material for the quench experiment. The starting mixture for the quench experiment contained 5.2 wt.% carbon (see Table 3.1), which is slightly enriched in Fe compared to  $\text{Fe}_3\text{C}$ .

#### 3.2.2. In-Situ X-Ray Diffraction Experiments

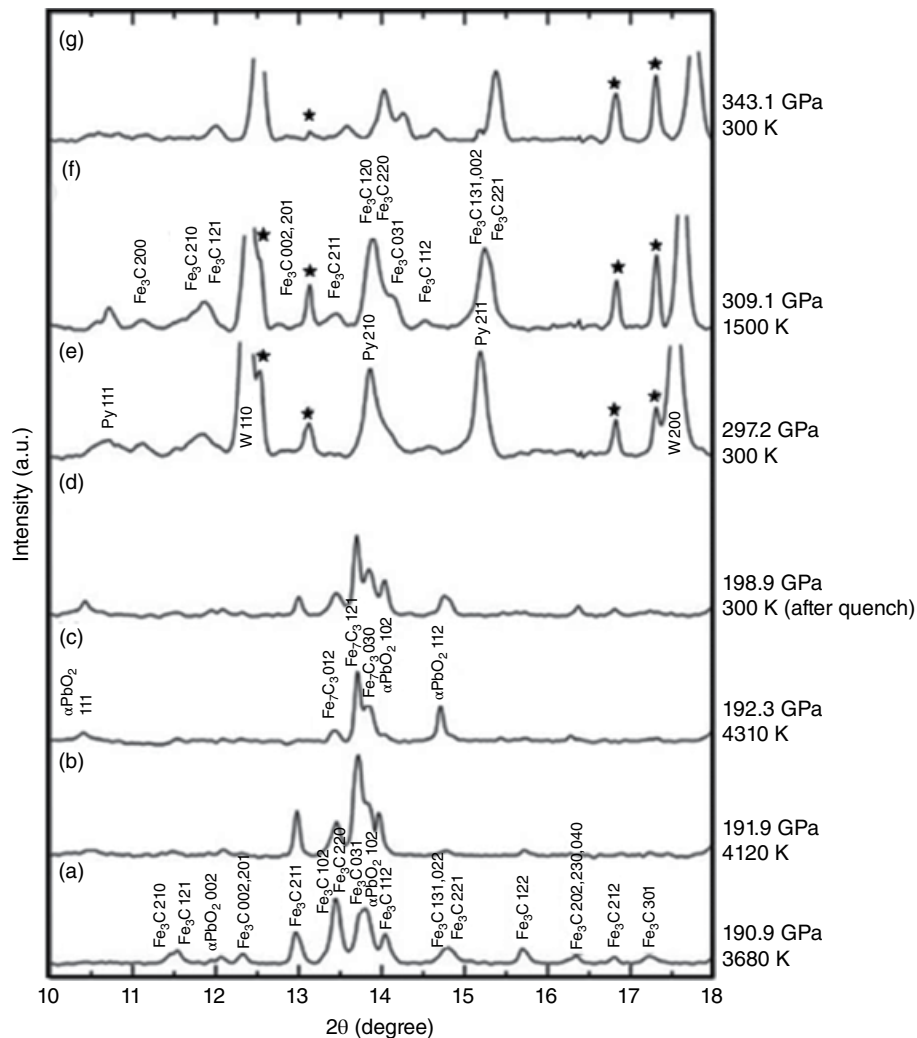
The in-situ X-ray diffraction experiments were conducted at the BL10XU beamline at the SPring-8 facility (Hyogo, Japan) (Ohishi et al., 2008). DAC experiments were performed using a symmetric-type diamond anvil cell. Diamond anvils with various culet sizes from 40 to 350  $\mu\text{m}$  were used, depending on the required experimental pressure conditions. Rhenium or tungsten gasket was pre-indented to a thickness of 10–70  $\mu\text{m}$ , and a 20–120  $\mu\text{m}$  diameter hole was drilled in the gasket to form a sample chamber. A foil from the powdered  $\text{Fe}_3\text{C}$  sample was prepared using a cold-compression technique. The sample foil was sandwiched between either NaCl or  $\text{SiO}_2$  glass layers and placed in the sample chamber. The NaCl or  $\text{SiO}_2$  layers served as a pressure-transmitting medium and as a thermal insulator.

The sample was heated using a double-sided laser heating technique employing an SPI fiber laser ( $\lambda = 1.070 \mu\text{m}$ ). The shape of the fibre laser beam was adjusted to a flat-top beam using the beam-shaping system at the BL10XU beamline. This technique enabled us to decrease the temperature gradient across the sample and achieve a homogenous heating of the area with a diameter of approximately 30  $\mu\text{m}$ . The temperature was determined by fitting the emission spectra from the surface of the heated sample to Planck's radiation law as a grey body formula using the typical wavelength range between 600 and 800 nm (Shen et al., 1996). The wavelength of the monochromatic X-ray beam and the distance between the sample and the X-ray detector were calibrated using X-ray diffraction patterns from  $\text{CeO}_2$  based on the double cassette method. The typical wavelength of the X-rays was in the range of 0.4140–0.4224 Å, which was determined with

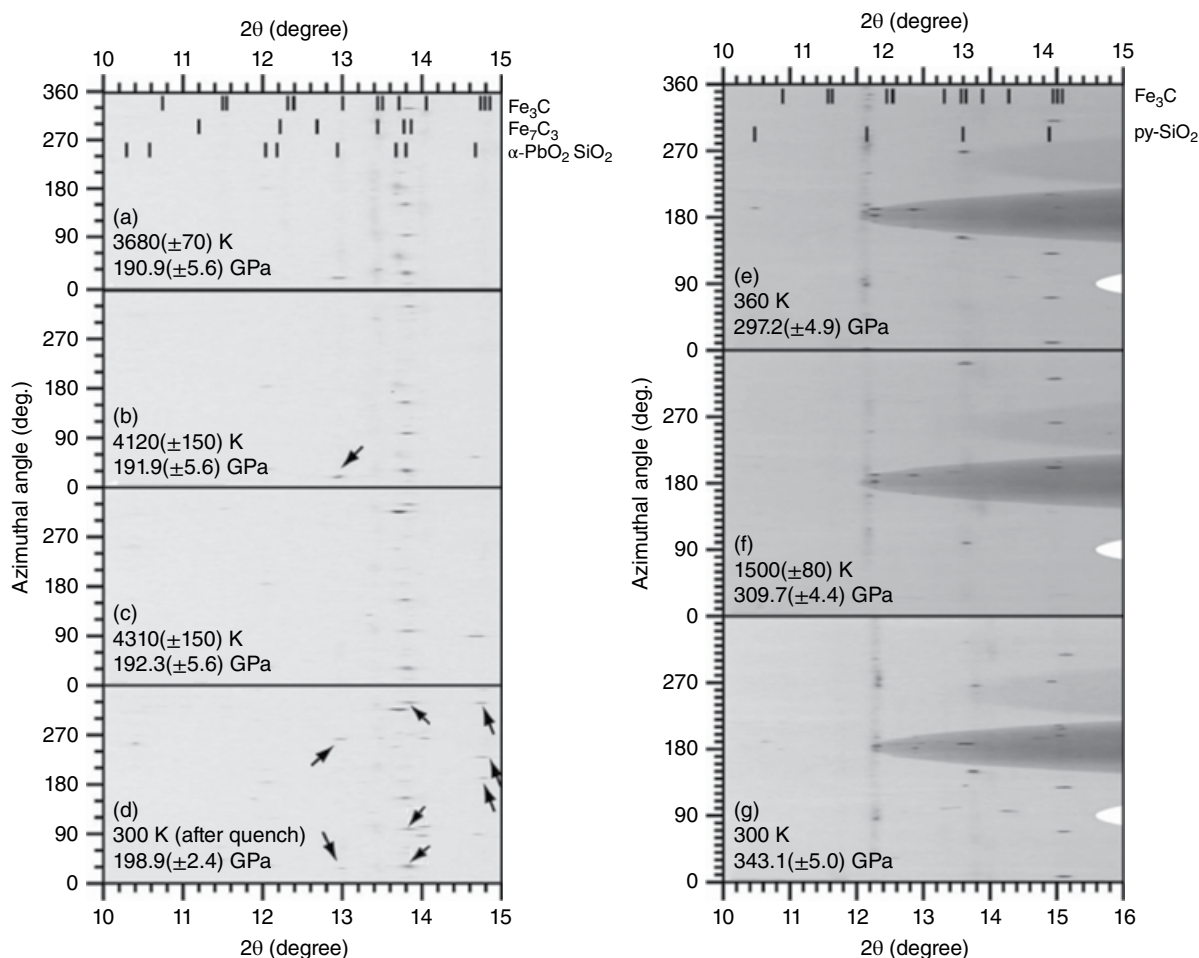
a precision of 0.04%. The X-ray beam was collimated to a diameter of 15  $\mu\text{m}$ . An IP detector (RAXIS-IV; Rigaku, Tokyo, Japan) and a CCD detector (SMART APEX; Bruker AXS, Madison, WI) were used to collect the angle-dispersive X-ray diffraction data. Exposure time for the IP and CCD was 3 min and 1–10 s, respectively. The examples of the diffraction patterns are given in Figures 3.1 and 3.2. The onset of melting of the sample was determined from the disappearance of the X-ray diffraction peaks and reappearance of the peaks after quenching at high pressure, as described in previous works (Kamada et al., 2010; Campbell et al., 2007; Morard et al., 2008).

Each integrated X-ray diffraction pattern, along with the  $2\theta$  angle (i.e., one dimensional X-ray diffraction profile), was analyzed using an IP analyzer and PD Indexer software package programmed by Y. Seto.

The experimental pressures were determined based on the lattice parameters of NaCl at ambient and high temperatures using the equation of state of NaCl with the B2 structure (Fei et al., 2007). An average of the lattice parameters at high temperature of the sample and those at ambient temperature at the diamond anvil surface was employed to determine the generated pressure using the procedure described by Campbell et al. (2009).



**Figure 3.1** Typical examples of X-ray diffraction patterns of  $\text{Fe}_3\text{C}$  at (a)–(d) 191–199 GPa and (e)–(g) 297–343 GPa, respectively. (a)  $\text{Fe}_3\text{C}$  was a stable subsolidus phase at 190 GPa and  $T > 3000$  K. (b) After further heating,  $\text{Fe}_3\text{C}$  peaks were observed up to 4120 K. (c) These peaks disappeared and  $\text{Fe}_7\text{C}_3$  peaks were observed at 4310 K. (d) After quenching, the  $\text{Fe}_3\text{C}$  peaks reappeared. This result indicates that  $\text{Fe}_3\text{C}$  incongruently melted to form  $\text{Fe}_7\text{C}_3$  and a liquid phase. (e) The  $\text{Fe}_3\text{C}$  peaks were broad before heating at 297 GPa. (f) During heating, the  $\text{Fe}_3\text{C}$  peaks became sharper at 1500 K. (g)  $\text{Fe}_3\text{C}$  was observed as a stable subsolidus phase up to 343 GPa. Key: \* denotes peaks derived from outside the sample chamber since the peak positions are fixed and do not shift with pressure and temperature. See electronic version for color representation of the figures in this book.



**Figure 3.2** IP (a, b, c, d) and CCD (e, f, g) data obtained at high pressure and temperature. Arrows in the figures are the diffraction peaks from  $\text{SiO}_2$  pressure medium ( $\alpha\text{-PbO}_2$  type  $\text{SiO}_2$  and py, pyrite type  $\text{SiO}_2$ ). These profiles correspond to one dimensional pattern shown in Figure 3.1. The peak positions of  $\text{Fe}_3\text{C}$ ,  $\text{Fe}_7\text{C}_3$ , and pyrite  $\text{SiO}_2$  are based on the equation of state of these phases by Sata et al. (2010), Chen et al. (2012), and Kuwayama et al. (2011), respectively. See electronic version for color representation of the figures in this book.

In addition, in the experiments with  $\text{SiO}_2$  glass as the pressure-transmitting medium, pressures were estimated using the equation of state of  $\text{Fe}_3\text{C}$  (Sata et al., 2010) with thermal expansion calculated by Vočadlo et al. (2002). The results of the experiments using two different pressure media were consistent with each other as shown in Table 3.2.

### 3.2.3. Quench Experiment and Sample Analysis

The sample sandwiched between  $\text{SiO}_2$  glass layers was compressed in a DAC and heated using a double-sided laser heating technique employing an SPI fiber laser ( $\lambda = 1.070 \mu\text{m}$ ) with a flat top beam. The pressure was determined at room temperature using the ruby fluorescence method (Dewaele et al., 2004) and/or the pressure shift of the edge of the  $T_{2g}$  Raman band of the culet of the

diamond anvil (Akahama & Kawamura, 2004). The pressure values determined by the two methods were consistent with each other. After decompression, the heated region of the recovered sample was cut by an FIB system (JEM-9320FIB; Jeol) (Miyahara et al., 2008). The texture of the prepared sample was observed using an FE-SEM (JSM-7001F; JEOL) at Tohoku University. We observed the coexistence of  $\text{Fe}_7\text{C}_3$  and a quenched melt phase in the recovered samples. Subsequently, the chemical compositions of the coexisting phases were analyzed using the wavelength-dispersive mode of an FE-EPMA (JXA-8530F; JEOL) at Tohoku University. An accelerating voltage of 15 kV and a beam current of 30 nA were employed to analyze the carbon content, and an LDE2H crystal in the EPMA was used to measure the carbon content in the sample. We determined the calibration curve from the relationship between the carbon content

**Table 3.2** Experimental conditions and observed phases.

RUN #	T (K)	P (GPa)	Observed Phases	VNaCl ( $\text{\AA}^3$ )	VSiO <sub>2</sub> ( $\text{\AA}^3$ )
<i>In-situ X-ray diffraction experiments</i>					
Fe3C350_061	300	68.0(9) <sup>a</sup>	$\text{Fe}_3\text{C}$ , NaCl(B2)	22.78(8)	
Fe3C350_063	1360(120)	72.7(24)	$\text{Fe}_3\text{C}$ , NaCl(B2)	22.67(2)	
Fe3C350_064	1710(200)	74.0(32)	$\text{Fe}_3\text{C}$ , NaCl(B2)	22.66(5)	
Fe3C350_065	1770(240)	73.2(33)	$\text{Fe}_3\text{C}$ , NaCl(B2)	22.75(12)	
Fe3C350_066	2090(70)	74.1(40)	$\text{Fe}_3\text{C}$ , NaCl(B2)	22.76(10)	
Fe3C350_067	2270(60)	74.5(44)	$\text{Fe}_3\text{C}$ , NaCl(B2)	22.78(10)	
Fe3C350_068	2450(70)	74.5(49)	$\text{Fe}_3\text{C}$ , NaCl(B2)	22.83(9)	
Fe3C350_069	2630(90)	74.7(53)	$\text{Fe}_3\text{C}$ , NaCl(B2)	22.87(9)	
Fe3C350_070	2810(80)	74.3(57)	$\text{Fe}_3\text{C}$ , NaCl(B2)	22.96(4)	
Fe3C350_071	3020(130)	72.5(61)	$\text{Fe}_7\text{C}_3$ (+L), NaCl(B2)	23.18(6)	
Fe3C350_072	3310(110)	73.4(68)	$\text{Fe}_7\text{C}_3$ (+L), NaCl(B2)	23.18(15)	
Fe3C350_073	3420(140)	75.3(71)	NaCl(B2)	23.05(1)	
Fe3C350_074	300	68.5(5)	$\text{Fe}_3\text{C}$ , $\text{Fe}_7\text{C}_3$ , NaCl(B2)	22.73(4)	
Fe3C3502_030	300	47.9(16)	$\text{Fe}_3\text{C}$ , NaCl(B2)	24.84(20)	
Fe3C3502_031	1500(50)	50.1(26)	$\text{Fe}_3\text{C}$ , NaCl(B2)	25.04(13)	
Fe3C3502_032	1820(50)	50.7(33)	$\text{Fe}_3\text{C}$ , NaCl(B2)	25.10(16)	
Fe3C3502_033	2010(50)	51.4(37)	$\text{Fe}_3\text{C}$ , NaCl(B2)	25.08(12)	
Fe3C3502_034	2270(90)	51.8(43)	$\text{Fe}_3\text{C}$ , NaCl(B2)	25.14(12)	
Fe3C3502_035	2430(110)	52.0(46)	$\text{Fe}_3\text{C}$ , NaCl(B2)	25.17(5)	
Fe3C3502_036	2550(100)	53.1(49)	$\text{Fe}_3\text{C}$ , NaCl(B2)	25.09(3)	
Fe3C3502_038	2790(100)	51.4(54)	$\text{Fe}_7\text{C}_3$ (+L), NaCl(B2)	25.41(20)	
Fe3C3502_039	3000(170)	50.4(58)	$\text{Fe}_7\text{C}_3$ (+L), NaCl(B2)	25.64(20)	
Fe3C3502_040	3340(150)	53.6(66)	NaCl(B2)	26.35(8)	
Fe3C3502_041	300	45.3(9)	$\text{Fe}_3\text{C}$ , $\text{Fe}_7\text{C}_3$ , NaCl(B2)	25.17(12)	
Fe3C130_038	300	122.0(9)	$\text{Fe}_3\text{C}$ , NaCl(B2)	19.48(4)	
Fe3C130_039	1900(80)	138.5(39)	$\text{Fe}_3\text{C}$ , NaCl(B2)	19.02(4)	
Fe3C130_040	2220(220)	142.2(47)	$\text{Fe}_3\text{C}$ , NaCl(B2)	18.92(2)	
Fe3C130_041	2260(200)	142.6(48)	$\text{Fe}_3\text{C}$ , NaCl(B2)	18.91(5)	
Fe3C130_042	2690(130)	143.5(59)	$\text{Fe}_3\text{C}$ , NaCl(B2)	18.94(19)	
Fe3C130_043	300	134.2(32)	$\text{Fe}_3\text{C}$ , NaCl(B2)	18.97(13)	
Fe3C130_044	2860(90)	151.3(64)	$\text{Fe}_3\text{C}$ , NaCl(B2)	18.67(19)	
Fe3C130_045	3600(200)	153.6(83)	$\text{Fe}_3\text{C}$ , NaCl(B2)	18.69(16)	
Fe3C130_046	3600(260)	154.5(83)	$\text{Fe}_3\text{C}$ , NaCl(B2)	18.65(17)	
Fe3C130_047	3660(150)	152.4(84)	$\text{Fe}_3\text{C}$ , NaCl(B2)	18.74(11)	
Fe3C130_048	3260(300)	154.7(74)	$\text{Fe}_3\text{C}$ , NaCl(B2)	18.60(6)	
Fe3C130_049	300	144.1(27)	$\text{Fe}_3\text{C}$ , NaCl(B2)	18.60(10)	
Fe3C130_050	300	146.3(34)	$\text{Fe}_3\text{C}$ , NaCl(B2)	18.52(12)	
Fe3C130_051	2980(200)	149.2(67)	$\text{Fe}_3\text{C}$ , NaCl(B2)	18.76(9)	
Fe3C130_052	3620(180)	154.7(83)	$\text{Fe}_3\text{C}$ , NaCl(B2)	18.65(2)	
Fe3C130_055	4270(460)	157.0(100)	$\text{Fe}_7\text{C}_3$ (+L), NaCl(B2)	18.66(5)	
Fe3C130_056	3910(260)	153.5(90)	$\text{Fe}_7\text{C}_3$ (+L), NaCl(B2)	18.73(14)	
Fe3C130_057	300	142.4(22)	$\text{Fe}_7\text{C}_3$ (+L), NaCl(B2)	18.66(8)	
Fe3C050_002	300	183.4(22)	$\text{Fe}_3\text{C}$ , NaCl(B2)	17.35(6)	
Fe3C050_003	1920(90)	209.1(41)	$\text{Fe}_3\text{C}$ , NaCl(B2)	16.83(1)	
Fe3C050_004	3070(130)	217.7(73)	$\text{Fe}_3\text{C}$ , NaCl(B2)	16.74(4)	
Fe3C050_005	2740(150)	226.1(64)	$\text{Fe}_3\text{C}$ , NaCl(B2)	16.51(4)	
Fe3C050_008	2020(50)	214.8(44)	$\text{Fe}_3\text{C}$ , NaCl(B2)	16.71(4)	
Fe3C050_009	2710(70)	219.6(63)	$\text{Fe}_3\text{C}$ , NaCl(B2)	16.66(2)	
Fe3C050_012	4100(150)	229.0(101)	$\text{Fe}_3\text{C}$ , NaCl(B2)	16.57(3)	
Fe3C050_014	3000(80)	231.5(71)	$\text{Fe}_3\text{C}$ , NaCl(B2)	16.42(9)	
Fe3C050_015	2810(40)	228.3(66)	$\text{Fe}_3\text{C}$ , NaCl(B2)	16.47(6)	
Fe3C050_016	300	217.4(13)	$\text{Fe}_3\text{C}$ , NaCl(B2)	16.50(3)	
Fe3C100_010	1980(40)	187.3(56)	$\text{Fe}_3\text{C}$ , SiO <sub>2</sub> ( $\alpha$ -PbO <sub>2</sub> type)		

(Continued)

**Table 3.2** (Continued)

RUN #	T (K)	P (GPa)	Observed Phases	VNaCl ( $\text{\AA}^3$ )	VSiO <sub>2</sub> ( $\text{\AA}^3$ )
Fe3C100_011	2860(70)	189.2(56)	Fe <sub>3</sub> C, SiO <sub>2</sub> ( $\alpha$ -PbO <sub>2</sub> type)		
Fe3C100_012	3680(70)	190.9(56)	Fe <sub>3</sub> C, SiO <sub>2</sub> ( $\alpha$ -PbO <sub>2</sub> type)		
Fe3C100_013	4120(150)	191.9(56)	Fe <sub>3</sub> C, SiO <sub>2</sub> ( $\alpha$ -PbO <sub>2</sub> type)		
Fe3C100_015	4310(150)	192.3(56)	Fe <sub>7</sub> C <sub>3</sub> (+L), SiO <sub>2</sub> ( $\alpha$ -PbO <sub>2</sub> type)		
Fe3C100_016	300	198.9(24)	Fe <sub>3</sub> C, Fe <sub>7</sub> C <sub>3</sub> , SiO <sub>2</sub> ( $\alpha$ -PbO <sub>2</sub> type)		
Fe3C040_018	300	297.2(49)	Fe <sub>3</sub> C, SiO <sub>2</sub> (pyrite type)		59.49(4)
Fe3C040_020	300	309.7(30)	Fe <sub>3</sub> C, SiO <sub>2</sub> (pyrite type)		58.72(19)
Fe3C040_022	1500(80)	309.7(44)	Fe <sub>3</sub> C, SiO <sub>2</sub> (pyrite type)		59.17(44)
Fe3C040_023	300	306.8(57)	Fe <sub>3</sub> C, SiO <sub>2</sub> (pyrite type)		58.81(18)
Fe3C040_025	300	313.1(31)	Fe <sub>3</sub> C, SiO <sub>2</sub> (pyrite type)		58.44(14)
Fe3C040_027	300	319.8(34)	Fe <sub>3</sub> C, SiO <sub>2</sub> (pyrite type)		58.50(13)
Fe3C040_029	1580(100)	325.8(23)	Fe <sub>3</sub> C, SiO <sub>2</sub> (pyrite type)		58.37(19)
Fe3C040_030	300	327.4(61)	Fe <sub>3</sub> C, SiO <sub>2</sub> (pyrite type)		58.18(15)
Fe3C040_032	300	321.6(83)	Fe <sub>3</sub> C, SiO <sub>2</sub> (pyrite type)		58.14(6)
Fe3C040_033	300	328.1(23)	Fe <sub>3</sub> C, SiO <sub>2</sub> (pyrite type)		57.94(10)
Fe3C040_034	300	324.8(31)	Fe <sub>3</sub> C, SiO <sub>2</sub> (pyrite type)		58.27(2)
Fe3C040_035	300	322.4(28)	Fe <sub>3</sub> C, SiO <sub>2</sub> (pyrite type)		58.16(13)
Fe3C040_038	300	322.8(27)	Fe <sub>3</sub> C, SiO <sub>2</sub> (pyrite type)		58.03(24)
Fe3C040_040	300	324.2(101)	Fe <sub>3</sub> C, SiO <sub>2</sub> (pyrite type)		58.18(44)
Fe3C040_042	300	333.6(69)	Fe <sub>3</sub> C, SiO <sub>2</sub> (pyrite type)		57.67(10)
Fe3C040_043	300	343.1(50)	Fe <sub>3</sub> C, SiO <sub>2</sub> (pyrite type)		57.30(37)
<i>Quenched experiment</i>					
Fe3C350lab_001	2850(200)	59.4(60) <sup>b</sup>	Fe <sub>3</sub> C, Fe <sub>7</sub> C <sub>3</sub> , Quenched L, SiO <sub>2</sub>		

Numbers in parentheses are uncertainties on the last digits.

<sup>a</sup> The pressures were determined by the equations of state B2 (Fei et al., 2007) for the runs using the NaCl pressure medium, and the equation of state of Fe<sub>3</sub>C (Sata et al., 2010) with the thermal expansion (Vočadlo et al., 2002) for the runs with the SiO<sub>2</sub> glass pressure medium.

<sup>b</sup> The pressure was determined by the pressure dependency of the edge of T<sub>2g</sub> Raman band of the diamond anvil (Akahama & Kawamura, 2004) and ruby fluorescence (Dewaele et al., 2004).

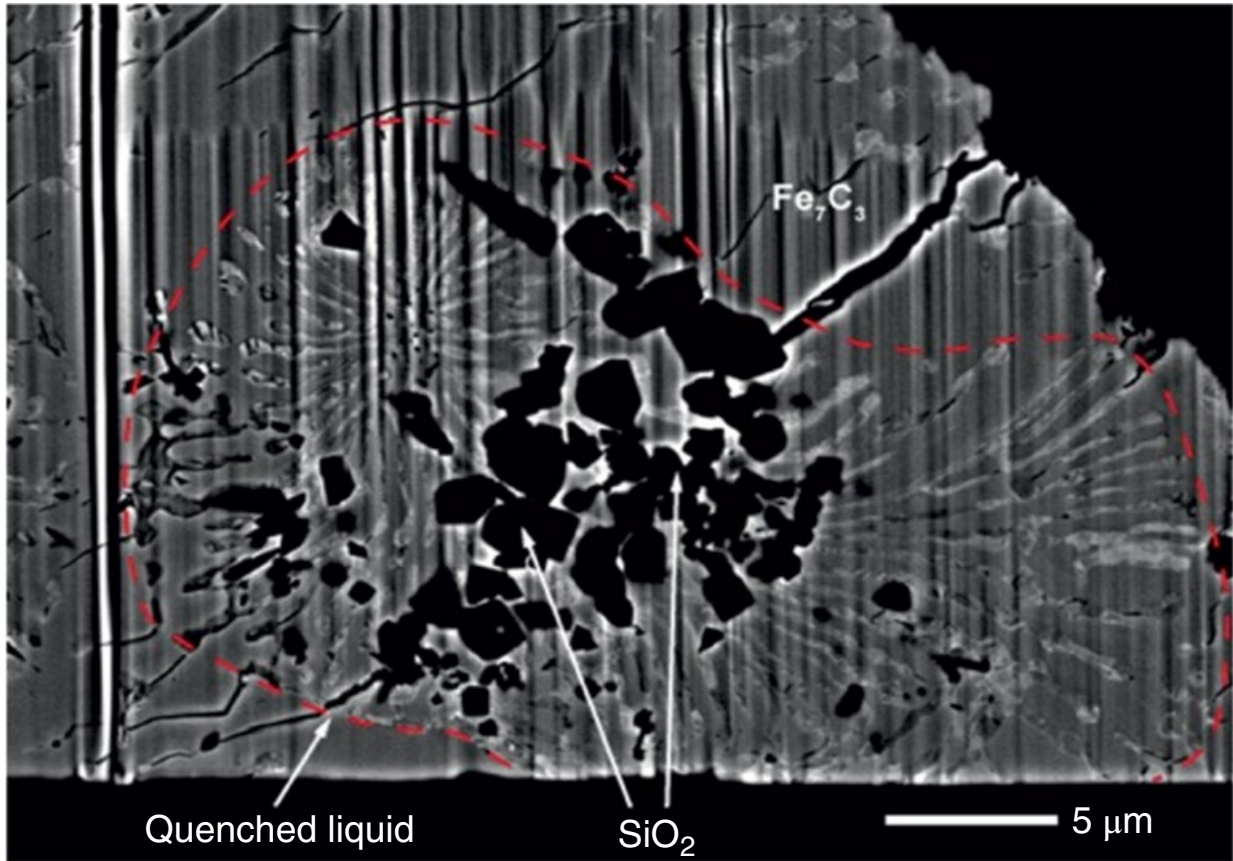
and the C K $\alpha$  count rates in the standards employed (Fe and Fe<sub>3</sub>C). The standard of Fe<sub>3</sub>C was synthesized at 3 GPa and 1273 K. Fe<sub>3</sub>C synthesized at this condition contains no compositional zoning nor impurities and is thus close to stoichiometry, according to Walker et al. (2013). An image of the recovered sample is shown in Figure 3.3 and the results of chemical analyses are summarized in Table 3.1.

### 3.3. RESULTS

#### 3.3.1. In-Situ X-Ray Diffraction Experiments

The experiments were carried out in the pressure range 50–340 GPa and the temperature range 300–4300 K. The diffraction patterns of Fe<sub>3</sub>C at pressures around 200 GPa and >300 GPa are shown in Figures 3.1 and 3.2. We observed Fe<sub>3</sub>C up to 191.9 GPa and 4120 K. After heating to higher temperatures, the X-ray diffraction peaks of Fe<sub>3</sub>C disappeared, and diffraction peaks assignable to Fe<sub>7</sub>C<sub>3</sub> were observed at 192.3 GPa and 4310 K. After quenching, the diffraction peaks of Fe<sub>3</sub>C reappeared. This

indicates clearly incongruent melting of Fe<sub>3</sub>C to Fe<sub>7</sub>C<sub>3</sub> and liquid, as was reported in previous studies at low pressure around 7–14 GPa (Nakajima et al., 2009; Litasov et al., 2013; Walker et al., 2013). At higher pressure conditions, we observed X-ray diffraction peaks ascribable to Fe<sub>3</sub>C up to 325 GPa at 1500 K and up to 343.1 GPa at 300 K (Figure 3.2). These results are consistent with preliminary data on the Fe<sub>3</sub>C stability at 360 GPa and temperatures up to 5500 K (Tateno et al., 2010), in which a carbide was formed by reaction of Fe with diamond anvils. Although Liu et al. (2016) reported that Fe<sub>3</sub>C decomposes to Fe and Fe<sub>7</sub>C<sub>3</sub> at pressures above 160 GPa, we clearly observed the existence of Fe<sub>3</sub>C up to 325 GPa and high temperature without decomposition, as shown in Figures 3.1 and 3.2. Chen et al. (2018) reported the sound velocities of Fe<sub>3</sub>C up to core pressures. Our results together with previous experiments (Gao et al., 2011; Chen et al., 2014; Chen et al., 2018) indicate that Fe<sub>3</sub>C with the cementite structure is likely to be stable in the inner core pressure and temperature conditions, although we need further detailed studies to confirm it. The experimental conditions and results are given in Table 3.2.



**Figure 3.3** A backscattered electron microscope image of a sample recovered from 59.4 GPa and 2850 K. The area enclosed by the red dashed line shows a quenched liquid phase.  $\text{SiO}_2$  was used as the pressure-transmitting medium. The quenched liquid is surrounded by  $\text{Fe}_7\text{C}_3$  grains. The region outside  $\text{Fe}_7\text{C}_3$  grains is composed of  $\text{Fe}_7\text{C}_3$  (dark) and  $\text{Fe}_3\text{C}$  (bright) grains with granular textures. The compositions of the quenched liquid and  $\text{Fe}_7\text{C}_3$  are given in Table 3.2. This image indicates incongruent melting of  $\text{Fe}_3\text{C}$ . See electronic version for color representation of the figures in this book.

### 3.3.2. Textual Observations and Chemical Analysis of the Recovered Sample

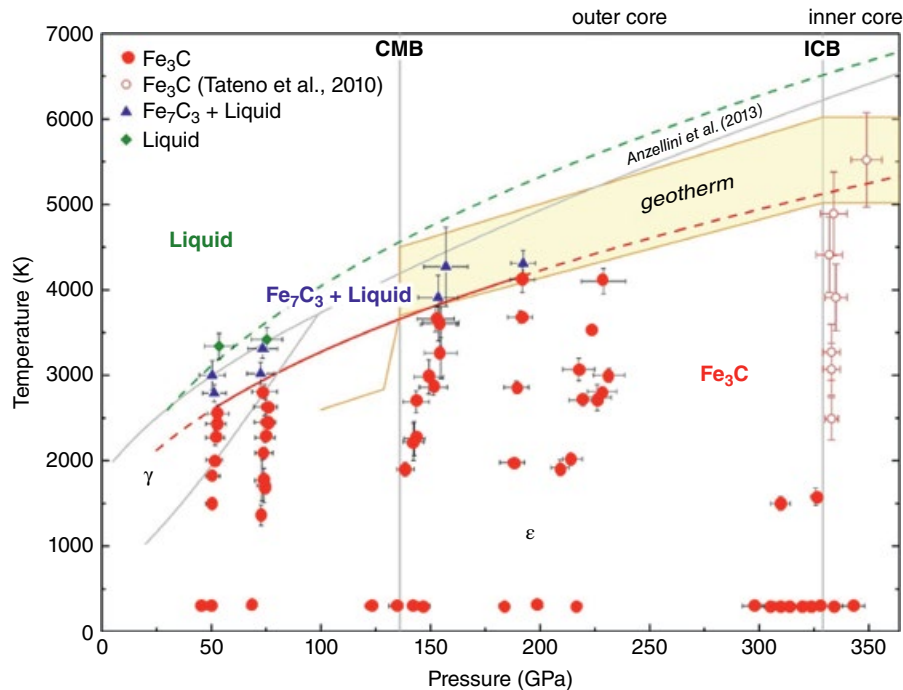
We performed textural observations of a recovered sample quenched from 59.4 GPa and 2850 K for a starting material with a bulk carbon content of 5.2 wt.%, which is slightly more enriched in Fe than the stoichiometric  $\text{Fe}_3\text{C}$ , as shown in Table 3.1. The quench texture of this run is shown in Figure 3.3. The carbon content in the quenched liquid phase was measured to be 4.7 wt.%, lower than the carbon content of the starting material. In addition, we observed  $\text{Fe}_7\text{C}_3$  as a liquidus phase. This result confirms incongruent melting of  $\text{Fe}_3\text{C}$  to  $\text{Fe}_7\text{C}_3$  and liquid at 59.4 GPa.

## 3.4. DISCUSSION

The experimental results are summarized in Figure 3.4. Our results of incongruent melting temperature of  $\text{Fe}_3\text{C}$  were fitted using Simon's equation as follows (Simon & Glatzel, 1929):

$$T_m = T_m^R \times \left( \frac{P - P^R}{A} + 1 \right)^{\frac{1}{C}}$$

where  $T_m$  and  $T_m^R$  are the melting temperature at an experimental pressure ( $P$ ) and a reference pressure ( $P^R$ ), respectively, and  $A$  and  $C$  are fitting parameters. This equation is employed for convenience of melting curve fitting following previous authors (Lord et al., 2009; Terasaki et al., 2011). The melting curve was fitted with the reference,  $P^R = 0$  GPa and  $T_m^R = 1500$  K GPa, which is the metastable incongruent melting temperature of  $\text{Fe}_3\text{C}$  at 1 bar (Benz & Elliott, 1961). The fitting parameters obtained here are  $A = 18.9 \pm 3.3$  and  $C = 2.4 \pm 0.2$ . The incongruent melting temperature of  $\text{Fe}_3\text{C}$  was estimated to be  $5130 \pm 180$  K at 330 GPa by extrapolation to the ICB pressure as shown in Figure 3.4. The fitted curve is consistent with the core isentropes and temperature at ICB estimated based on melting of mantle materials and



**Figure 3.4** Phase diagram of  $\text{Fe}_3\text{C}$ . The solid circles, triangles, and diamonds represent  $\text{Fe}_3\text{C}$ ,  $\text{Fe}_7\text{C}_3$  + liquid, and liquid, respectively. The open circles show  $\text{Fe}_3\text{C}$  as products of the reaction between iron and the diamond anvil, as observed by Tateno et al. (2010). The grey lines show the melting and phase boundary of Fe (Anzellini et al., 2013). The solid curve is the solidus temperature fitted using Simon's equation (Simon & Glatzel, 1929). The curve represents the approximate boundaries between  $\text{Fe}_3\text{C}$  and  $\text{Fe}_7\text{C}_3$  + liquid. The curve was fitted with the reference  $P^R = 0$  GPa and  $T_m^R = 1500$  K GPa (Benz & Elliott, 1961), and parameters  $A = 18.9 \pm 3.3$  and  $C = 2.4 \pm 0.2$ . The liquidus curve is shown as a dashed curve, which is expressed by the parameters  $A = 18.9$  and  $C = 2.4$ , which are assumed to be the same as the parameters of the solidus curve, and  $T_m^R = 1798$  K and  $P^R = 7.7$  GPa (Terasaki et al., 2014). The solidus temperature at the ICB is estimated to be 5130 K. The shaded area represents the temperature distribution of the core (Nimmo, 2015). See electronic version for color representation of the figures in this book.

energetics of the core, that is, heat flux from the core (Nimmo, 2015).

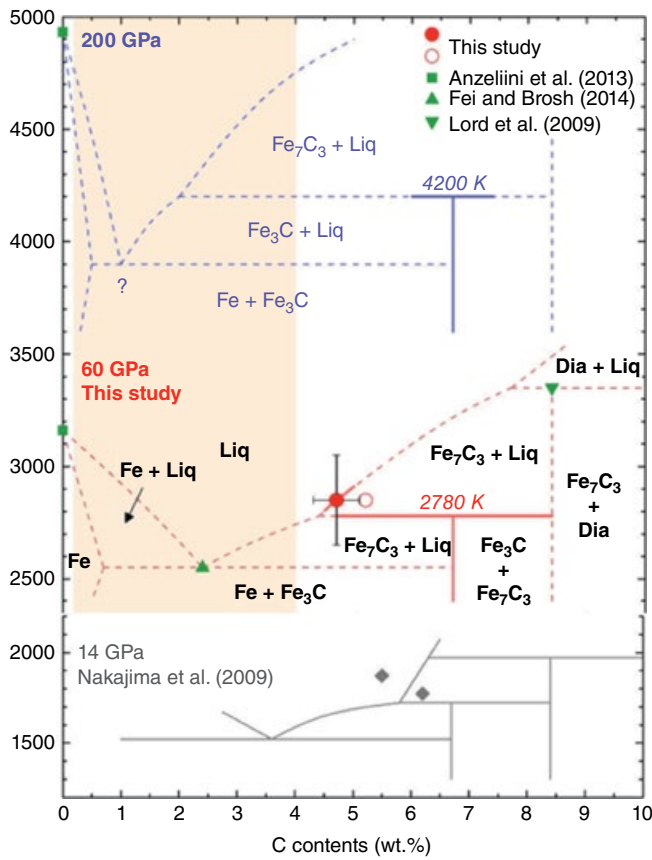
Figure 3.5 shows the phase and melting relationships of the Fe-C system from 14 GPa (Nakajima et al., 2009) to 200 GPa. The composition of the liquid formed by incongruent melting of  $\text{Fe}_3\text{C}$  at 60 GPa determined in this work (Table 3.1) is Fe-rich in composition compared to that at 14 GPa. The compositions of the peritectic liquids coexisting with  $\text{Fe}_7\text{C}_3$  shift toward the Fe-rich side at pressures from 14 GPa to 60 GPa. This result indicates that the Fe- $\text{Fe}_3\text{C}$  eutectic composition will also change to Fe-rich in composition, as has been shown in previous studies (Lord et al., 2009; Fei & Brosh, 2014) expanding compositional fields of liquidus  $\text{Fe}_3\text{C}$  and  $\text{Fe}_7\text{C}_3$ .

Lord et al. (2009) proposed that both hcp-Fe and  $\text{Fe}_7\text{C}_3$  are stable as subsolidus phases and are candidates for the inner core. However, our results clearly reveal that  $\text{Fe}_3\text{C}$  is a stable carbon-bearing compound, although it melts incongruently into  $\text{Fe}_7\text{C}_3$  and liquid at temperatures above  $5130 \pm 180$  at 330 GPa (Figure 3.4). Therefore,

both  $\text{Fe}_3\text{C}$  and  $\text{Fe}_7\text{C}_3$  are potential stable carbon-bearing phases in the inner core.

Several authors have estimated the carbon content in the core. Wood (1993) estimated the concentration of carbon in the core to be 2–4 wt.% based on high solubility of carbon in liquid Fe and high abundance of carbon in C1 chondritic meteorites. McDonough (2003) estimated a carbon content of 0.2 wt.% from his estimation of bulk Earth composition and mass balance calculations between the mantle and core. Fiquet et al. (2009) estimated the carbon content in the core to be about 1 wt.% based on the sound velocity of  $\text{Fe}_3\text{C}$  and the preliminary reference Earth model (PREM) inner core. Mookherjee et al. (2011) estimated the maximum carbon content in the inner core to be 1.5 wt.% based on sound velocity measurements and ab initio calculations on  $\text{Fe}_7\text{C}_3$ . According to recent experiments at 1–3 GPa and 1773–2073 K, the partition coefficient of carbon between metal and silicate melts varies between 500 and 5400, which is different from previous estimations and





**Figure 3.5** The Fe-rich portion of the Fe-C phase diagram up to 200 GPa inferred from our experiments in comparison with experiments and thermodynamic calculations at 14 GPa (Nakajima et al., 2009). The solid and open circles represent the carbon content of the quenched melt coexisting with  $\text{Fe}_7\text{C}_3$  and the composition of the starting material in the quenching experiment at 60 GPa, respectively. The grey diamond symbols show the melt compositions at 14 GPa (Nakajima et al., 2009). The melting temperatures of Fe, solid squares, were based on the data from Anzellini et al. (2013). The eutectic composition at 60 GPa, a solid triangle, was estimated to have about 2.4 wt.% C based on the pressure shift of the Fe- $\text{Fe}_3\text{C}$  eutectic composition by Fei and Brosh (2014). The peritectic temperature was estimated by the Simon's equation fitting of the experimental data (Figure 3.2). The shaded area represents the possible bulk carbon content in the Earth's core (Wood, 1993; McDonough, 2003; Fiquet et al., 2009). Compared to the Fe-C phase diagram at 14–60 GPa, the composition of the quenched melt coexisting with  $\text{Fe}_7\text{C}_3$  is likely to be shifted toward the Fe-rich side with increasing pressure (Nakajima et al., 2009; Fei & Brosh, 2014). See electronic version for color representation of the figures in this book.

indicates strong partitioning to the metal, comparable with partitioning of highly siderophile elements (Chi et al., 2014). If the Earth was accreted from C1 chondrite parental bodies with high carbon content, up to 4 wt.% of carbon can be easily concentrated in the Earth's core.

Therefore, the carbon content in the Earth's core is likely to be in the range 0.2–4 wt.%. The equation of state of  $\text{Fe}_7\text{C}_3$  showed that the density of the inner core can well be explained by a single phase of  $\text{Fe}_7\text{C}_3$  (Nakajima et al., 2011) or a mixture of 90–60 vol.% of  $\text{Fe}_7\text{C}_3$  and 10–40% of hcp-Fe (Chen et al., 2012). The equation of state of  $\text{Fe}_3\text{C}$  determined previously (Sata et al., 2010; Litasov et al., 2013) indicates similar compression behaviors of  $\text{Fe}_3\text{C}$  to  $\text{Fe}_7\text{C}_3$ . Thus, the inner core can be explained by  $\text{Fe}_7\text{C}_3$  or  $\text{Fe}_3\text{C}$  within the experimental uncertainty of the equation of state, assuming the ICB temperature  $\sim 5000$  K. Finally, sound velocity measurements of  $\text{Fe}_7\text{C}_3$  (Chen et al., 2014; Prescher et al., 2015) indicate that it can explain low  $V_S$  of the inner core without application of specific crystallization conditions (Mattesini et al., 2013; Yoshida et al., 1996) or premelting effects (Martorell et al., 2013). Indeed,  $\text{Fe}_3\text{C}$  is the next plausible compound to explain low  $V_S$  in the inner core (Gao et al., 2011; Gao et al., 2008).

The previous and present melting relationships of the Fe- $\text{Fe}_3\text{C}$  system shown in Figure 3.5 indicate that the peritectic liquid coexisting with  $\text{Fe}_7\text{C}_3$  shifts toward the Fe-rich side with increasing pressure. The eutectic liquid composition of the system is likely to shift toward a similar direction with increasing pressure. If Fe carbide is a liquidus phase during crystallization of the inner core, the initial crystallizing phase from the liquid core may be  $\text{Fe}_7\text{C}_3$ , followed by  $\text{Fe}_3\text{C}$ , and then by a mixture of hcp-Fe and  $\text{Fe}_3\text{C}$  at the latest stage. Crystallization of hcp-Fe and  $\text{Fe}_3\text{C}$  from the eutectic liquid provides no compositional convection in the outer core, because no light element is expelled by the crystallization. The latent heat due to crystallization will only be the energy source to create geodynamo in the outer core.

Thus, the distribution of these phases in the inner core could account for its internal structure, as revealed by seismology of the innermost inner core (Ishii & Dziewonski, 2002; Cao & Romanowicz, 2007). Our results suggest the innermost inner core of  $\text{Fe}_7\text{C}_3$ , which is consistent with a recent compression study (Nakajima et al., 2011; Chen et al., 2012). According to elasticity of  $\text{Fe}_7\text{C}_3$  and  $\text{Fe}_3\text{C}$  determined by ab initio calculations, both carbides are highly anisotropic (Mookherjee et al., 2011; Mookherjee, 2011) and could explain anisotropy in the inner core even better than hcp-Fe. Caracas (2017), on the other hand, argued that the anisotropy of hcp-iron increases with increasing carbon content. Lai et al. (2018) showed experimentally a strong anisotropy of  $\text{Fe}_7\text{C}_3$  up to 80 GPa and 800 K, and argued that high temperature may significantly influence the elastic anisotropy. A recent seismological study (Wang et al., 2015) suggested that both the inner core and the innermost inner core have different types of seismic anisotropy. If  $\text{Fe}_3\text{C}$  and  $\text{Fe}_7\text{C}_3$  crystallized in the core, they could cause the anisotropic structure within the inner core. We should notice

that detailed quantitative arguments on carbide layering in the inner core with its anisotropy is not possible at present due to insufficient experimental data on the phase relations of the Fe-C system under the inner core conditions and should be evaluated in future studies.

Crystallization of carbon-bearing phases would concentrate carbon in the inner core, resulting in a depletion of carbon in the outer core. Other light elements, such as H, O, Si, and S need to be present to satisfy the observed density of the outer core, since the outer core has a smaller density compared to the inner core. Although the multicomponent systems are not yet studied at high pressure to reveal liquidus phases during the inner core crystallization, carbides are very promising candidates if we compare melting temperatures of different compounds under the core conditions (FeSi by Lord et al., 2010; Fe<sub>72.5</sub>Si<sub>27.5</sub> by Fischer et al., 2011; Fe<sub>90.1</sub>Si<sub>9.9</sub> by Asanuma et al., 2010; Fe<sub>75</sub>O<sub>5</sub>S<sub>20</sub> by Terasaki et al., 2011). In the Fe-C-S system, iron carbide would be the liquidus phase, which could coexist with a sulfur-rich liquid, although the experiments are limited to 7 GPa (Dasgupta et al., 2009) and need to be confirmed at higher pressures.

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### AUTHOR CONTRIBUTIONS

ST, EO, TS, IM, SK, and TS performed high-pressure experiments. ST, SO, MM, YI, KS, and NA carried out chemical analyses. NH and YO supported the in-situ XRD experiments at SPring-8. ST, EO, and TS wrote the paper. All authors discussed the results and commented on the manuscript.

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